

Force Controllers for daVinci in AMBF Simulator

Team

Farid Tavakkologhaddam Sapan Agrawal Kartik Patath Hao Yang Tianyu Zhu **Instructor** Prof. Gregory Fischer

Introduction & Background

- Da Vinci Research Kit (dVRK):
 - An Open teleoperated surgical robotic system consisting of master and slave sides
- Patient Side Manipulator (PSM):
 - Comprised of two tool manipulator arms and one endoscope
 - 7 DOF for dexterous and natural hand manipulation
- Master Tool Manipulator (MTM):
 - Comprised of two haptic manipulator arms
 - 7 DOF for dexterous and natural hand manipulation
- Control challenges
 - Lack of feedback from haptic devices
 - No compliant controller available for either the PSM or MTM



a) Clinical da Vinci system



b) PSM arms of dVRK [1,2]



c) dVRK MTM [5]

MTM Kinematic Model

- Overall structure rotates about the vertical axis of J1 of an angle θ1
- Revolute joints with axes J2, J2', J2'' and J3 form a 2-DOF parallelogram mechanism
- Two actuated joints of the parallelogram are those about axes J2 (angle θ2) and J3 (angle θ3)
- the axes J4, J5, J6 and J7 intersect in the same point and correspond to revolute joints with angles θ4, θ5, θ6 and θ7
- All the joints are actuated by a motor, with the exception of the two revolute joints of the parallelogram about axes J2' and J2"



Master tool Manipulator (MTM) kinematics with Denavit-Hartenberg frames [7]

G. A. Fontanelli, F. Ficuciello, L. Villani and B. Siciliano, "Modelling and identification of the da Vinci Research Kit robotic arms," 2017 IEEE/RSJ International Conference on Intelligent Robots and Systems (IROS), Vancouver, BC, 2017, pp. 1464-1469.

AMBF (Asynchronous Multi Body Framework)

• AMBF is a simulator capable of simulating multiple robots asynchronously in real time

and Interventional

Medicine Laboratory

 It also provides real time haptic interaction with robots via haptic devices such as dVRK's Master Tool Manipulator (MTM), Razer Hydras

Why AMBF!?

- Support for closed loop/parallel mechanisms (such as the dVRK MTM)
- Built-in position (PID) and effort (torque) controller
- Compatible with ROS and Python client
- Readily available robot models such as dVRK and KUKA lbr
- Uses YAML file format, a human-readable file format, for model description!

Robot representation (YAML vs. URDF)

YAML

- "YAML is not a Markup Language"
- Non-hierarchical model (i.e each link has its own parent and child)
- Can define closed loop mechanisms
- Can be used as a universal description format

URDF

- Unified Robot Definition Format
- Hierarchical model (i.e single parent and multiple children)
- No support closed loop mechanisms
- Not a universal format

YAML file description

• Body

BODY link1: name: link1 mesh: link1.STL mass: 1.0 collision margin: 0.001 scale: 1.0 location: orientation: {p: -0.0, r: 0.0, y: 0.0} position: {x: 0.0, y: 0.0, z: -1.197} inertial offset: orientation: {p: 0, r: 0, y: 0} position: {x: 0.0, y: -0.017, z: 0.134} friction: {rolling: 0.01, static: 0.5} damping: {angular: 0.95, linear: 0.95} restitution: 0 collision groups: [0] color components: ambient: {level: 1.0} diffuse: {b: 0.0054, g: 0.2702, r: 0.8} specular: {b: 1.0, g: 1.0, r: 1.0} transparency: 1.0

• Joint

JOINT base-link1: name: base-link1 parent: BODY base child: BODY link1 parent axis: {x: 0.0, y: 0.0, z: 1.0} parent pivot: {x: 0.0, y: 0.0, z: 0.103} child axis: {x: 0.0, y: 0.0, z: 1.0} child pivot: {x: 0.0, y: 0.0, z: 0.0} joint limits: {high: 2.094, low: -2.094} controller: {D: 2.0, I: 0, P: 1000.0} type: revolute

RBDL:

- Rigid Body Dynamics Library is a C++ based dynamics library
- Available for use in python using the wrapper module
- Contains essential rigid body dynamics algorithms
 - Articulated Body Algorithm (ABA) for forward dynamics
 - Dynamics modeling using Recursive Newton-Euler Algorithm (RNEA)
 - Composite Rigid Body Algorithm (CRBA) for the efficient computation of the joint space inertia matrix
- Comprehensive support for both kinematic and dynamics modeling
 - Forward and inverse kinematics
 - Handling of external constraints such as closed-loop contacts
 - Forward and inverse dynamics, Jacobian, inertia, ...

Challenge: NO Documentation ! ! !

YAML to RBDL model

- For calculation of the dynamics, RBDL takes "rbdl.model()" object as an input to access all the required information such as:
 - Mass, inertia, center of mass location, ...
 - Description of the kinematic chain of the robot model
 - Joint and contact types
- Parameters from a YAML file need to be parsed into an RBDL model
- This conversion is handled by a custom-made parser class which constructs the RBDL model by receiving the YAML file as an input!

YAML to RBDL parser



def YamlToRBDLmodel(data, Bodies, Joints):

for i in range(0, no_of_bodies):
 # Creating of the transformation matrix between two adjacent bodies
 trans = robl.SpatialTransform()
 if i=0 :
 trans.r = lo.9, 0.0, 0.0;
 # print("R ish", trans.E);
 trans.r = [0.0, 0.0, 0.0];
 # print("T ish", trans.r);
 print("T ish", trans.r);
 else:
 # get parent and child aces of the pair
 child_axis = dicttovec(child_axes[i-1][0])
 parent_axis = dicttovec(child_axes[i-1][0])
 # Find the rotation matrix between child and parent
 r_mat = rot_matrix_from_vecs(mathutils.Vector(child_axis), mathutils.Vector(parent_axis))
 # print("R is", r_mat_n)
 trans.r = prent("R is", r_mat_n)
 # print("R is'', trans.F);
 print("R is'', trans.F);
 print("R is'', trans.F);
 print("R is'', trans.F);
 rotation = print("T ish", trans.F);
 # print("R is'', trans.F);
 # print("R ish", trans.F);

Creating intertia matrix with jost principle intertia values
I_x = inertia_valij[0]
I_y = inertia_valij[1]
I_z = inertia_valij[2]
inertia_matrix = np.array([I_x, 0, 0], [0, I_y, 0], [0, 0, I_z]])
Creating each body of the robot
body = robl.Body.fromMassComInertia(mass[i], com_val[i], inertia_matrix)

Specifying joint Type if i == 0: joint_type = joint_fixed else: joint_type = joint_rot_z # joint_type = rbdl.Joint.fromJointType(joint_nam print("joint type is", joint_type);

Adding body to the model to create the complete robo model.AppendBody(trans, joint_type, body) # print(i)

eturn model

Gravity compensation

• Used to overcome torques generated by the robot's masses

Generalized equation of motion equation

Using inverse dynamics given zero velocity and acceleration terms, we have:

- Purpose
 - To test the accuracy of the dynamics model
 - Is further used for the impedance controller
- Criteria for the implementation
 - The robot should hold any given position
 - No need for use of any other controllers (meaning accurate model)

 $\vec{\tau} = M\left(\vec{q}\right)\vec{\ddot{q}} + V\left(\vec{q}, \dot{\vec{q}}\right) + G\left(\vec{q}\right) + \vec{\tau}_{d}$

 $\tau = G(q)$

M: inertia matrix *V*: velocity dependent matrix r_d : disturbance torques *G*: gravity matrix

Gravity compensation (contd.)

Gravity compensation for the KUKA arm:



Gravity compensation

Gravity compensation for the MTM:



a) Serial MTM arm



b) Full MTM arm

Impedance controller

Goal:

Control the relationship between the robot motion and the contact force as required for the task.

Benefits:

- Simultaneous force and motion control
- Suitable for tasks involving human-robot interaction



Impedance Control for Soft Robots*

P. Song, Y. Yu and X. Zhang, "Impedance Control of Robots: An Overview," 2017 2nd International Conference on Cybernetics, Robotics and Control (CRC), Chengdu, 2017, pp. 51-55
 *Keppler, Manuel, et al. "Elastic Structure Preserving Impedance (ESπ) Control for Compliantly Actuated Robots." 2018 IEEE/RSJ International Conference on Intelligent Robots and Systems (IROS). IEEE, 2018.

Mathematical Formulation

- D_d : Damping Matrix
- K_d : Stiffness Matrix
- M_d :Desired Inertia Matrix
- m : Inertia Matrix in Task Space, m = $(J^T)^{-1} M(q) J^T$

M(q): Inertia Matrix in Joint Space

Reference: RBE-501 Robot Dynamics Lecture 13 Robotics 2 by Prof. Prof. Alessandro De Luca: <u>http://www.diag.uniroma1.it/deluca/rob2_en.php</u>

Trajectory Tracking via Impedance Control on KUKA-LBR



KUKA-LBR tracking linear trajectory along X axis



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Rejection to External Perturbation

Force at the end Effector for different stiffness



Gains:

Control of Force and Motion Relationship



motion along Z axis



KUKA-LBR Tip Position/Velocity Within/out Disturbance, Kp=0.3/0.5/0.7: Desired vs. Real

x-axis unit: ms y-axis unit: m



x-axis unit: ms y-axis unit: m/ms

MTM impedance controller with Kp=0.3/0.5/0.7

X_desired = -0.4 m ~ +0.35 m V_desired = 0.5 m/s



Drawback: system easily being disturbed or unstable

MTM Tip Position/Velocity Within/out Disturbance, Kp=0.3/0.5/0.7: Desired vs. Real



x-axis unit: ms y-axis unit: m/ms

x-axis unit: ms y-axis unit: m

Performance comparison (PD VS. Impedance)

Compliance to obstacles:



Impedance controller with low stiffness in the x direction

- Ability to set desired stiffness of the end-effector in the cartesian space
- Low stiffness provides lower interaction force at the end-effector
- Desired when operating in environments where robot interaction with the surrounding environment is of importance



PD controller

- Lack of compliance when encountering an obstacle
- Relatively easier implementation
- Desirable in applications where fast response and short settling times are required

Summary

- \checkmark Derive the dynamics models of MTM and KUKA arms
- J Implement the impedance controller on MTM and KUKA arms
 - Fully automated method to parse YAML file into model in RBDL
- Two fully documented working robot model examples with working dynamics and controllers for the AMBF simulator
- New function for the python API to get inertia of the bodies from AMBF
 - Additional controller implementation gravity compensation and CTC

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References

- [1] <u>www.Intuitive.com</u>
- [2] https://sites.google.com/site/davidvgealy/research
- [3] https://github.com/WPI-AIM/ambf
- [4] https://www.kuka.com
- [5] https://research.intusurg.com/index.php/Main_Page

Thank you!



Inverse dynamics controller

Computed torque controller (CTC)

- Given desired position, velocity, acceleration compute the required joint torques
- Error terms are added with the desired acceleration
- Purpose
 - Test the full dynamics model
 - Used for comparison with the impedance controller to highlight the differences



$$\vec{\tau} = M\left(\vec{q}\right) \ddot{\vec{q}} + V\left(\vec{q}, \dot{\vec{q}}\right) + G\left(\vec{q}\right) + \vec{\tau}_{d}$$

$$u = M(q)a_q + V(q, \dot{q}) + G(q)$$

 \vec{u}_{q} = The set output (i.e. motor torque) $\vec{a}_{q} = \vec{q}_{d}$ = The second derivative of the input command trajectory

$$a_q = q_d(t) - K_p e - K_v e \qquad e = q - q_d$$
$$e = q - q_d$$

 K_p : diagonal stiffness matrix K_p : diagonal damping matrix e: position error de: velocity error

$$u = M(q) \Big[\ddot{q}_{d}(t) - K_{P}e - K_{V}\dot{e} \Big] + V(q, \dot{q}) + G(q)$$